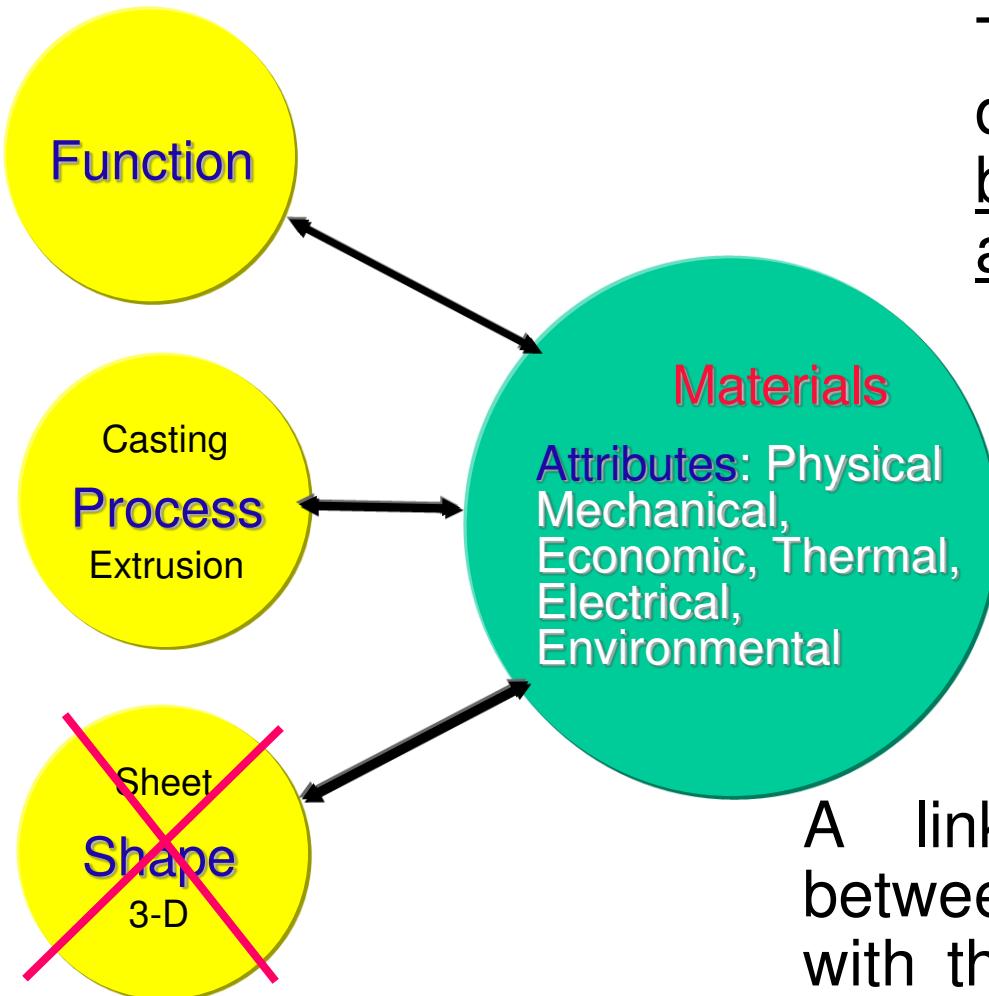


Chapter Three (Part 1)



Materials Performance Indices (Without Shape)

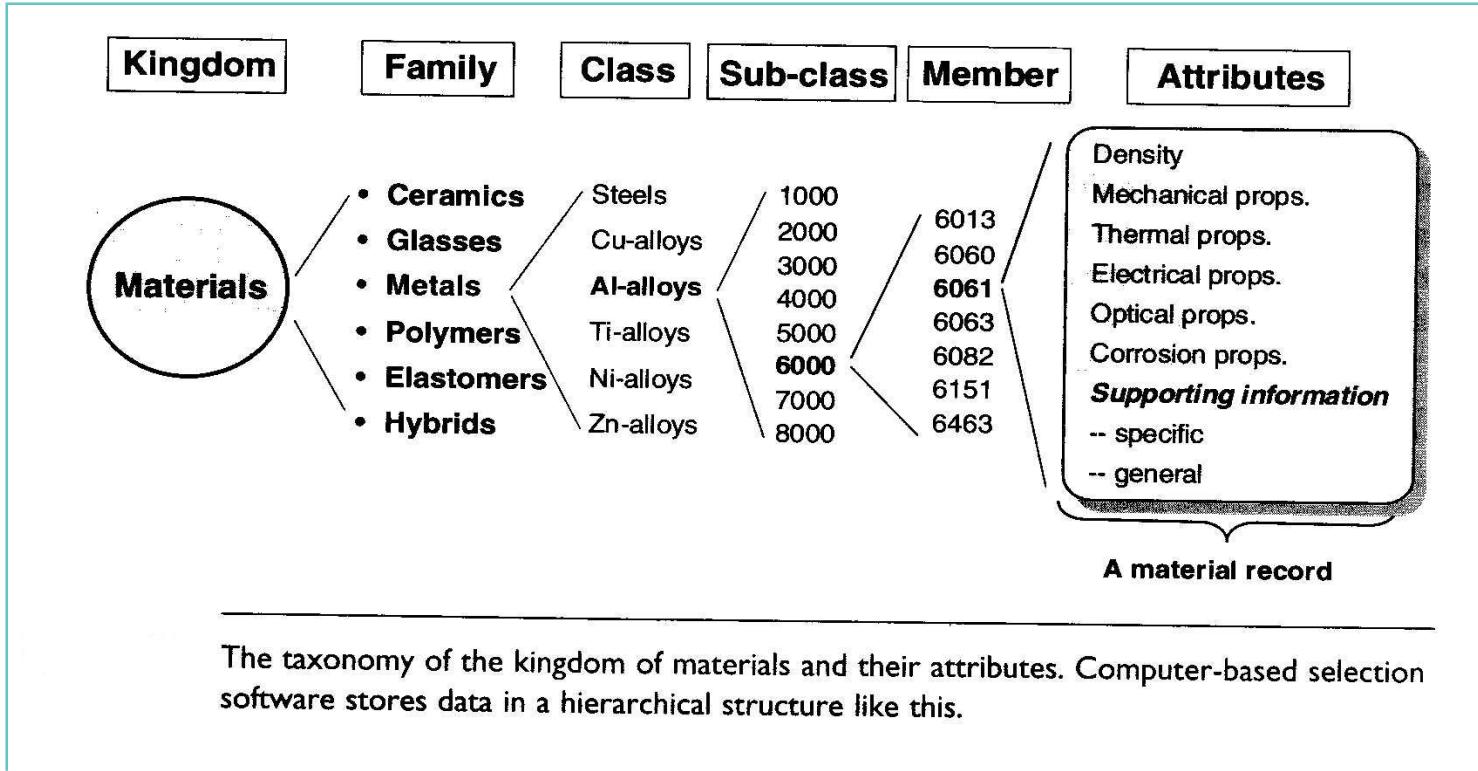


The selection of a material depends on the interaction between the **MATERIAL** and **FUNCTION**.

A link must be established between **MATERIAL**, **FUNCTION** with the **PROCESS** and **SHAPE** playing an important role

Adapted from M.F. Ashby

MATERIAL ATTRIBUTES



- An engineering component has:
(boundary condition for Materials Selection)

1. **Function**: to carry load, transmit heat, contain a pressure, etc..

What does the component do?

2. **Objectives**: as cheap as possible, light, safe, strong, etc...

What is to be Maximised or Minimised?

3. **Constraints**: subject to constraints such as carry load without failure, certain dimensions are fixed, cost is within limits etc...

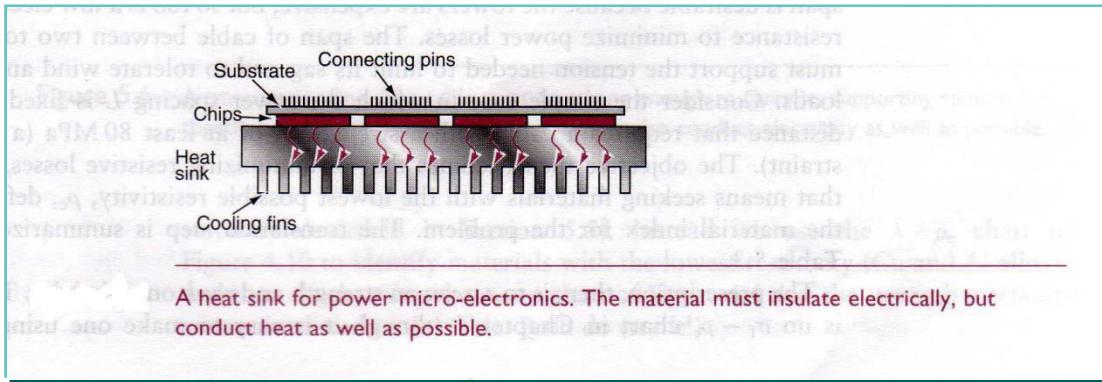
- *What non-negotiable conditions are to be met? (Rigid)*
- *What negotiable but desirable conditions? (Soft)*

4. **Free Variables**: materials choice, cross-section area, thickness, and length are free

Which design variables are free? (variables which can be changed)

e.g. an engineering component has:
(boundary condition for Materials Selection)

Heat Sink for hot microchips



A heat sink for power micro-electronics. The material must insulate electrically, but conduct heat as well as possible.

Function

Objective

Constraints

Free variables

Heat sink

Maximize thermal conductivity

- Materials must be good insulator
- All dimensions are specified

Choice of material

- Two concepts are used in the selection procedure:

1. Materials Performance Index

Combination of materials properties that characterise the performance of a material in a given application (Ashby)

2. Materials Selection Charts

Plots of materials properties that form the maximising factors

Two concepts are used in the selection procedure:

1) Material Performance Indices

- Performance of a component/structure is specified by:
 1. *Functional requirements (function) (F) e.g. carry loads, transmit energy, store energy etc.*
 2. *Geometry, (G)*
 3. *Materials properties, (M)*

Performance:

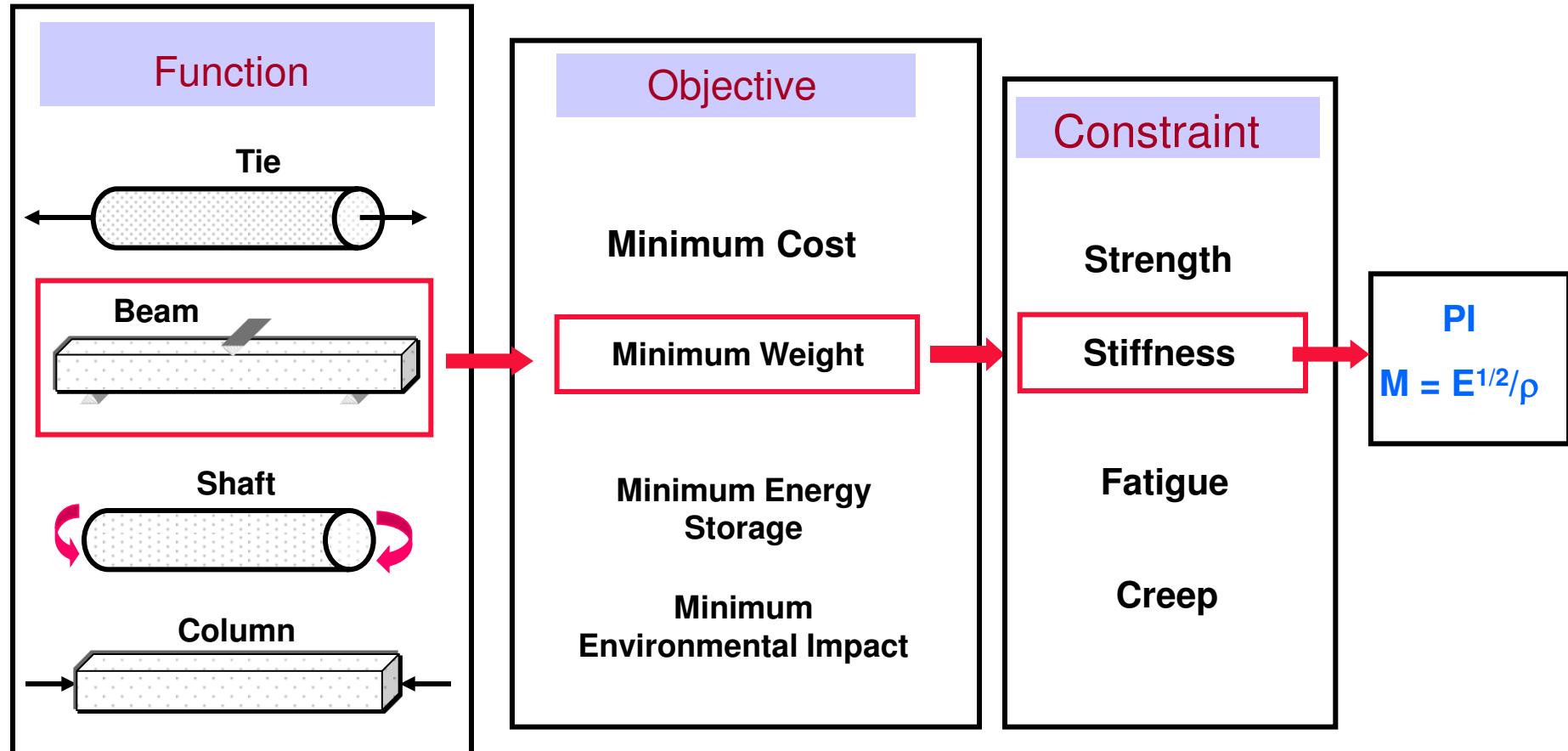
$P = f [(\text{functional requirements, } F); (\text{geometry, } G); (\text{materials properties, } M)]$

$$P = f(F, G, M)$$

- Optimum design is selection of a material which **maximise** (strength, stiffness) or **minimise** (weight, cost) the performance, P .
- In many cases, the function, geometry and materials properties are independent of each other and are said to be separable.

$$P = f_1(F) \times f_2(G) \times f_3(M)$$

- Which means that the optimum selection of a material is independent of the details of the design. It is the same for all geometries and values of functional requirements.
- Performance is maximised by maximising $f_3(M)$ and is called ***“Performance Index, M”***



Specification of **Function**, **Objective** and **Constraint** leads to a material performance index M . (after Ashby, 1999)

Functions and Constraints

Maximise (Stiffness)

Tie (tensile strut)

Stiffness, length specified, section area free

$$E/\rho$$

Beam (loaded in bending)

Stiffness, length, shape specified, section area free

$$E^{1/2}/\rho$$

Stiffness, length, height specified, width free

$$E/\rho$$

Stiffness, length, width specified, height free

$$E^{1/3}/\rho$$

Panel (flat plate, loaded in bending)

Stiffness, length, width specified, thickness free

$$E^{1/3}/\rho$$

Panel (flat plate, buckling failure)

Collapse load, length and width specified, thickness free

$$E^{1/3}/\rho$$

After M.F. Ashby

Strength (not
stiffness)

Functions and Constraints

Maximise (Strength)

Tie (tensile strut)

Stiffness, length specified, section area free

$$\sigma_f / \rho$$

Beam (loaded in bending)

Stiffness, length, shape specified, section area free

$$\sigma_f^{2/3} / \rho$$

Stiffness, length, height specified, width free

$$\sigma_f / \rho$$

Stiffness, length, width specified, height free

$$\sigma_f^{1/2} / \rho$$

Panel (flat plate, loaded in bending)

Stiffness, length, width specified, thickness free

$$\sigma_f^{1/2} / \rho$$

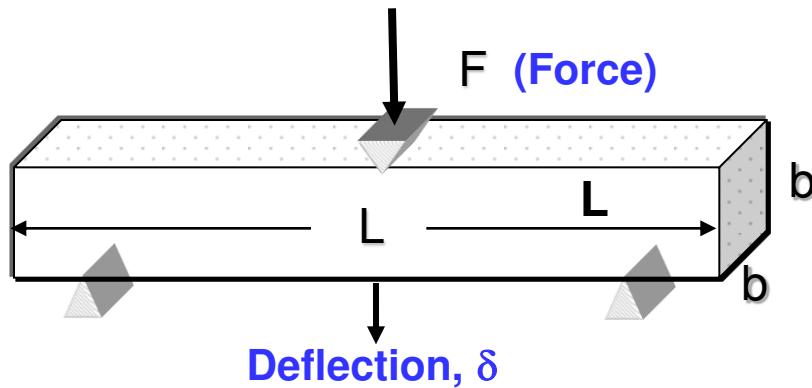
Panel (flat plate, buckling failure)

Collapse load, length and width specified, thickness free

$$\sigma_f^{1/2} / \rho$$

After M.F. Ashby

Example 1: Performance Index for a light, stiff beam



- **FUNCTION :** Beam (bending)
- **OBJECTIVE :** minimise mass (weight)
- **CONSTRAINT(S):** Stiffness is $S = F/\delta$ (must not deflect more than δ)
- **FREE VARIABLE(S):** Cross-sectional area (A), material

- The beam of square section, loaded in bending. Its stiffness is $S = F/\delta$ (must not deflect more than δ)
- Constraint on stiffness is given by:
- For a square cross section, “ I ” is given by:
- The mass (**Objective**), m , is given by:

$$S = \frac{F}{\delta} \geq \frac{C_1 EI}{l^3} \quad (1)$$

$$I = \frac{b^4}{12} = \frac{A^2}{12} \quad (2)$$

$$m = Al\rho \quad (3)$$

- The free variable is the cross section area, $A = b^2$
- Combining equations (1), (2) and (3), the free variable, A , can be eliminated and we then obtain:

$$m \geq \left(\frac{12S}{C_1 l} \right)^{1/2} l^3 \left(\frac{\rho}{E^{1/2}} \right) \quad (4)$$



F G M  PERFORMANCE INDEX

The best materials for a light, stiff beam are those with the smallest value of $\rho/E^{1/2}$.
Therefore, to minimize the mass

$$M = \frac{E^{1/2}}{\rho}$$

PERFORMANCE INDEX

OBJECTIVE : minimize mass (weight)

Example 1: Performance Index for a light, stiff beam

- A **light** and **stiff** beam (*cross section free*) is one with the largest:

$$M = \frac{E^{1/2}}{\rho}$$

- If *height is free*, the material index is:

$$M = \frac{E^{1/3}}{\rho}$$

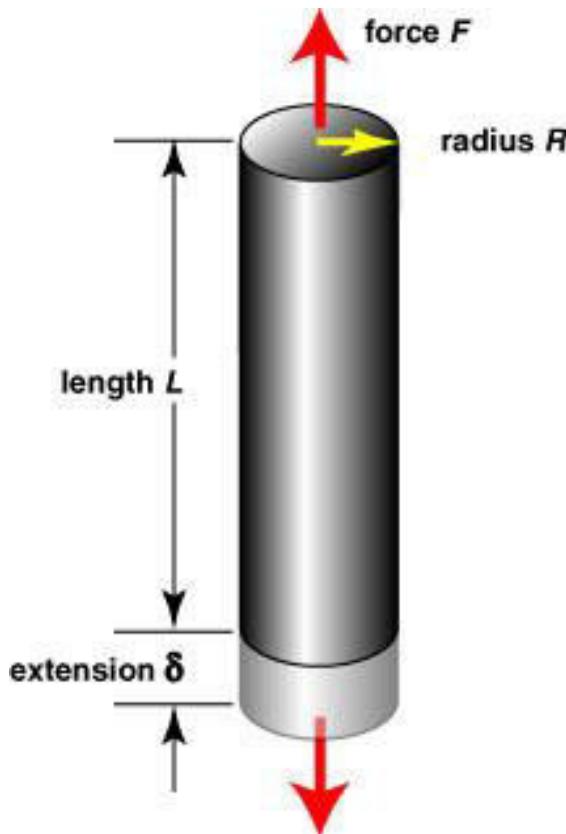
- If the *width is free*, the material index is:

$$M = \frac{E}{\rho}$$

Steps in deriving a “performance Index”

1. Identify the primary **FUNCTION**
2. Develop an equation for the **OBJECTIVE** (objective function): e.g; weight, cost, etc... (to be maximised or minimised). Objective function contains one or more free variables.
3. Identify the **CONSTRAINTS** (which must be met), rank them in order of importance
4. Identify the **FREE VARIABLES** (unspecified)
5. Develop equations for the constraints (no failure, no buckling, cost below target...)
6. Eliminate the free variable(s) in the objective equation using the constraints.
7. Group the variables into 3 groups: F, G, M
8. Read-off the grouping of materials properties, (called the “**PERFORMANCE INDEX**”), which maximise the objective

Example 2: Performance Index for a light and stiff cylindrical tie



- A tie is loaded in **tension (FUNCTION)** (stiffness limited design at lowest mass)
- **Specified dimensions (CONSTRAINTS):** F , L and δ .
- **Free variable:** cross-sectional area, A .
- **Mass (OBJECTIVE):**

$$m = Al\rho \quad (1)$$

- Deflection:

$$\delta = L\varepsilon = L\frac{\sigma}{E} = L\frac{F}{AE} \quad (2)$$

- This gives the area A;

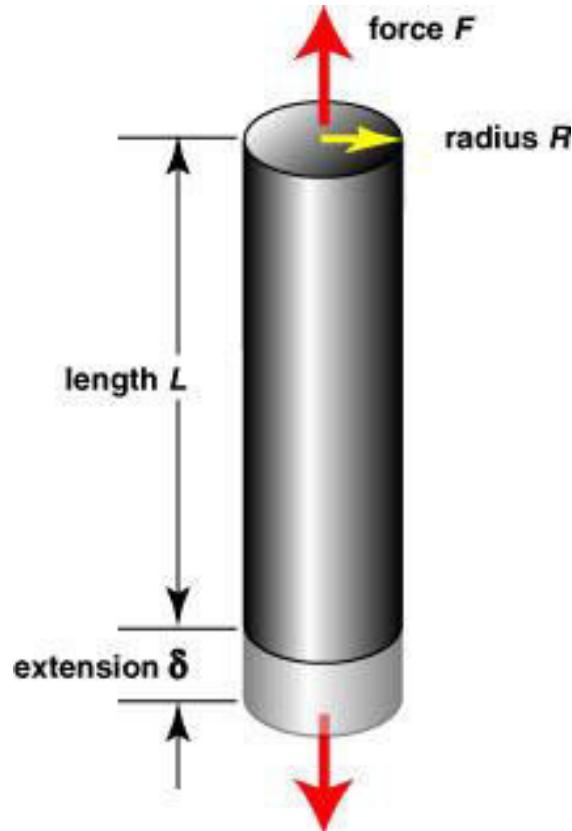
$$A = \frac{FL}{\delta E} \quad (3)$$

- Substituting (3) into (1) gives:

$$m = \frac{FL}{E\delta} L\rho = \frac{FL^2}{\delta} \frac{\rho}{E} \quad (4)$$

- To minimise the weight (mass) the material performance index

$$M = \frac{E}{\rho} \quad (5)$$



should be maximised and the $E - \rho$ chart will be used to select the optimum material

Example 3: Performance Index for a light & strong cylindrical tie

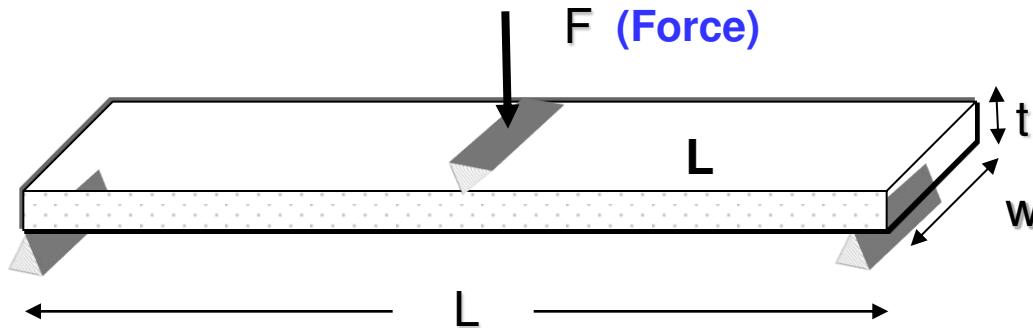
- A tie is loaded in tension (**FUNCTION**), carry load, F without failure
- Specified dimensions (**CONSTRAINTS**): F , L , *failure* (σ_f)
- **FREE VARIABLE**: cross-sectional area, A .
- Reduce Mass (**OBJECTIVE**):

$$m = Al\rho \quad (1)$$

- The tie must carry load F without failure: $\sigma_f = \frac{F}{A}$ (2)

$$m = \frac{F}{\sigma_f} l\rho \quad \longrightarrow \quad M = \frac{\sigma_f}{\rho}$$

Example 4: Performance Index for a light and stiff panel (fixed width)



FUNCTION

Panel (beam): bending

OBJECTIVE

Reduce weight: $m = AL\rho = w t L \rho$ (1)

CONSTRAINT

Stiffness $S = F/\delta = CEI/L^3$, $I = w t^3/12$ (2)

FREE VARIABLE

Thickness, t

We get the free variable, t, from Eq. (2),

$$S = \frac{CEI}{L^3} = \frac{CEwt^3}{12L^3}$$



$$t = \left(\frac{12SL^3}{CEw} \right)^{1/3}$$

Replacing t into Eq. 1, we get:

$$m = \left(\frac{12Sw^2}{C} \right)^{1/3} L^2 \left(\frac{\rho}{E^{1/3}} \right)$$

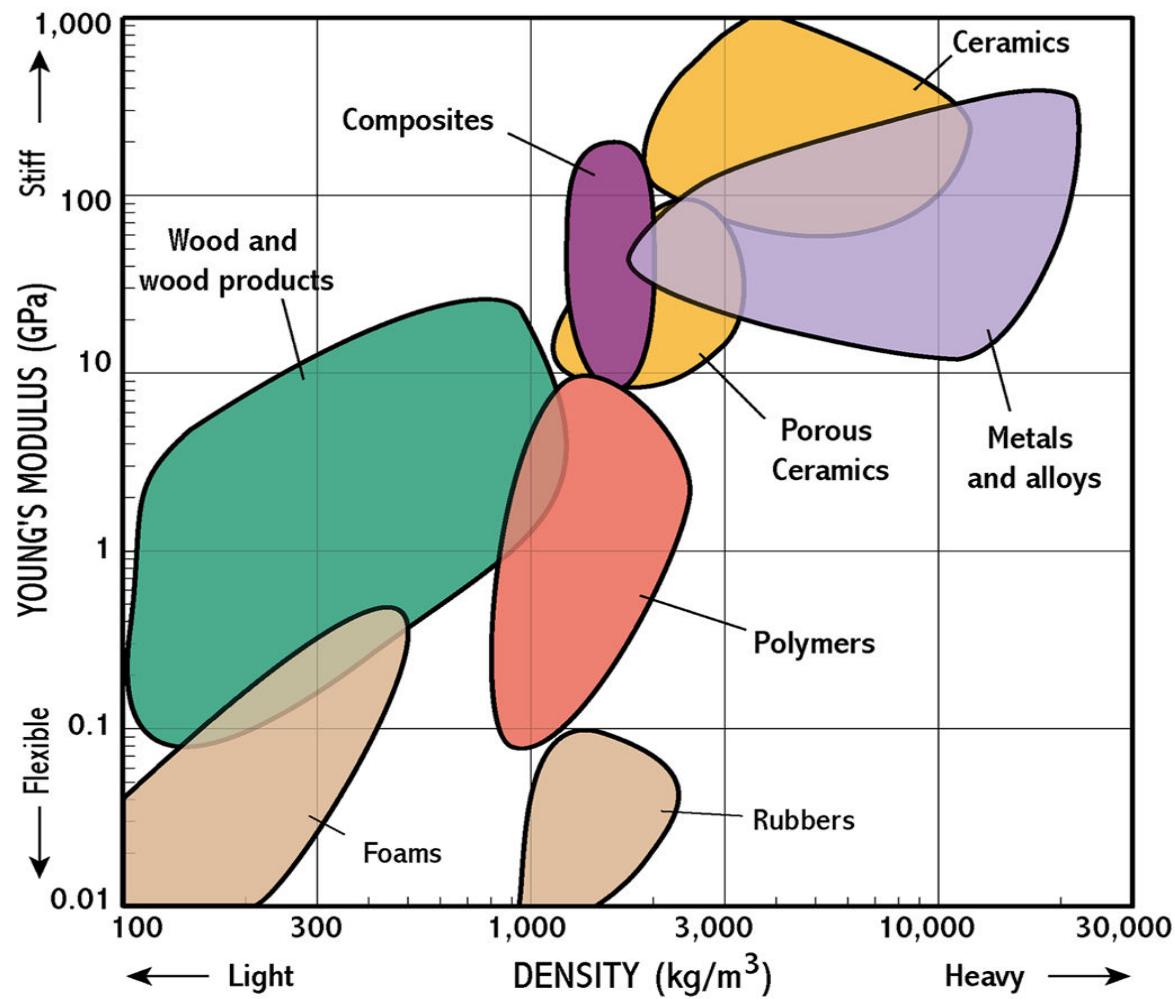
We select materials with the largest

$$M = \frac{E^{1/3}}{\rho}$$

Two concepts are used in the selection procedure:

2) Materials Selection Charts

- The selection of the optimum material is made more simple by the use of “*Materials Selection Charts*”
- Materials selection charts are plots of the properties that form the maximising factors.
- The performance index is made up of 2 properties (e.g; E & ρ). The material selection chart is then created with axis (log by default) of E and ρ .



After M.F. Ashby

- The performance index, M , plots as a diagonal line on the chart. Its slope is very important.
- For the performance index $M = E/\rho$. We take log;

$$\log E = \log M + \log \rho$$

- A line of slope 1 on the chart describes the index; its position is determined by the value of M .
- For $M = E^{1/2}/\rho$ and $E^{1/3}/\rho$, gives lines with slope 2 and 3 respectively.
- They are called “*design guidelines*”

Young's modulus - Density

Technical ceramics

Composites

Metals

Natural materials

Longitudinal
wave speed

10^4 m/s

Rigid polymer
foams

Foams

10^3 m/s

10^2 m/s

0.01

0.1

Density, ρ (Mg/m³)

10

MFA, 04

Young's modulus, E (GPa)

1000

100

10

1

10^{-1}

10^{-2}

10^{-3}

10^{-4}

Technical ceramics

Composites

Metals

Natural materials

Polymers and elastomers

Guidelines for minimum mass design

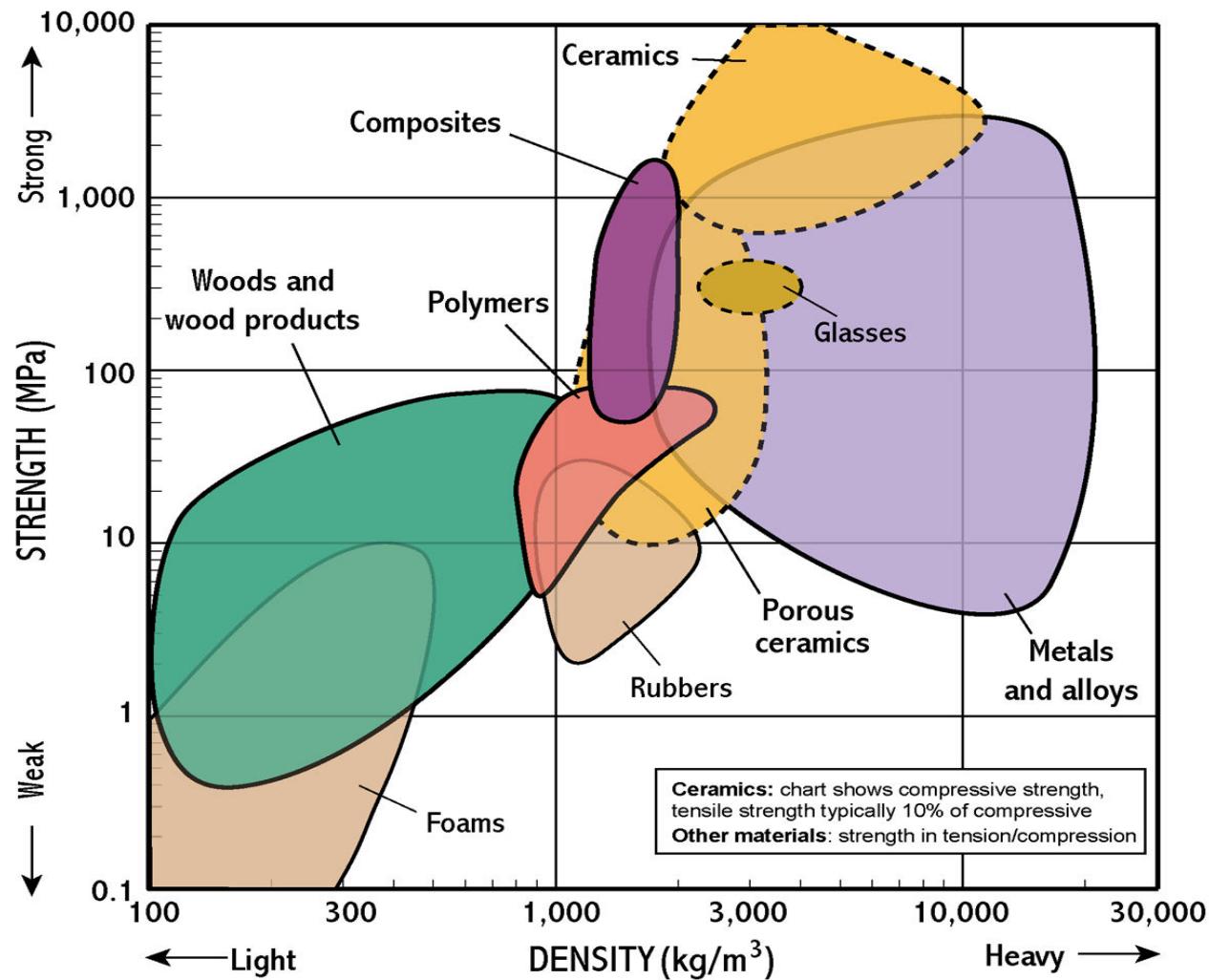
$E/\rho^{1/3}$

$E/\rho^{1/2}$

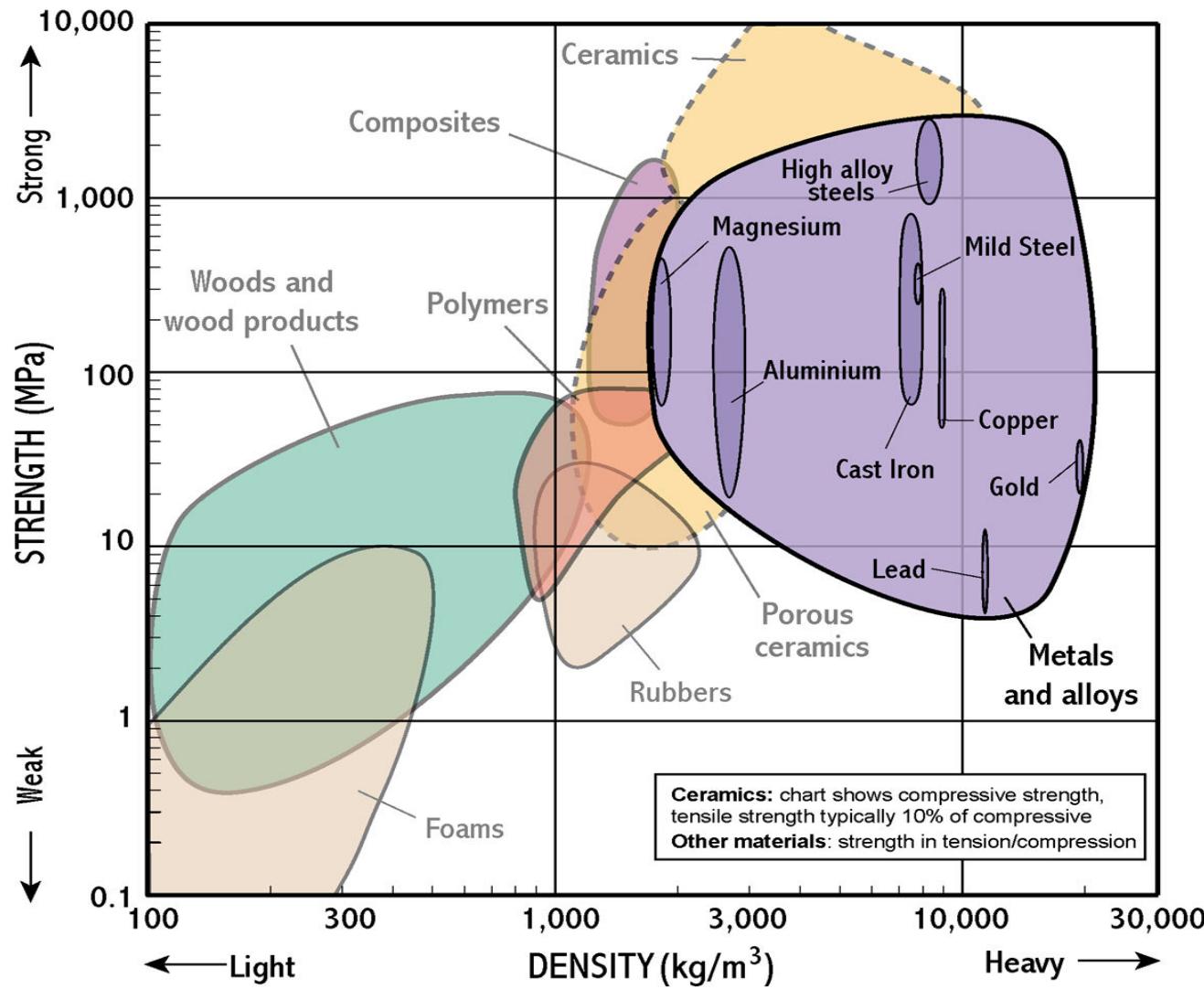
E/ρ

$E/\rho^{1/3}$

$E/\rho^{1/2}$



After M.F. Ashby

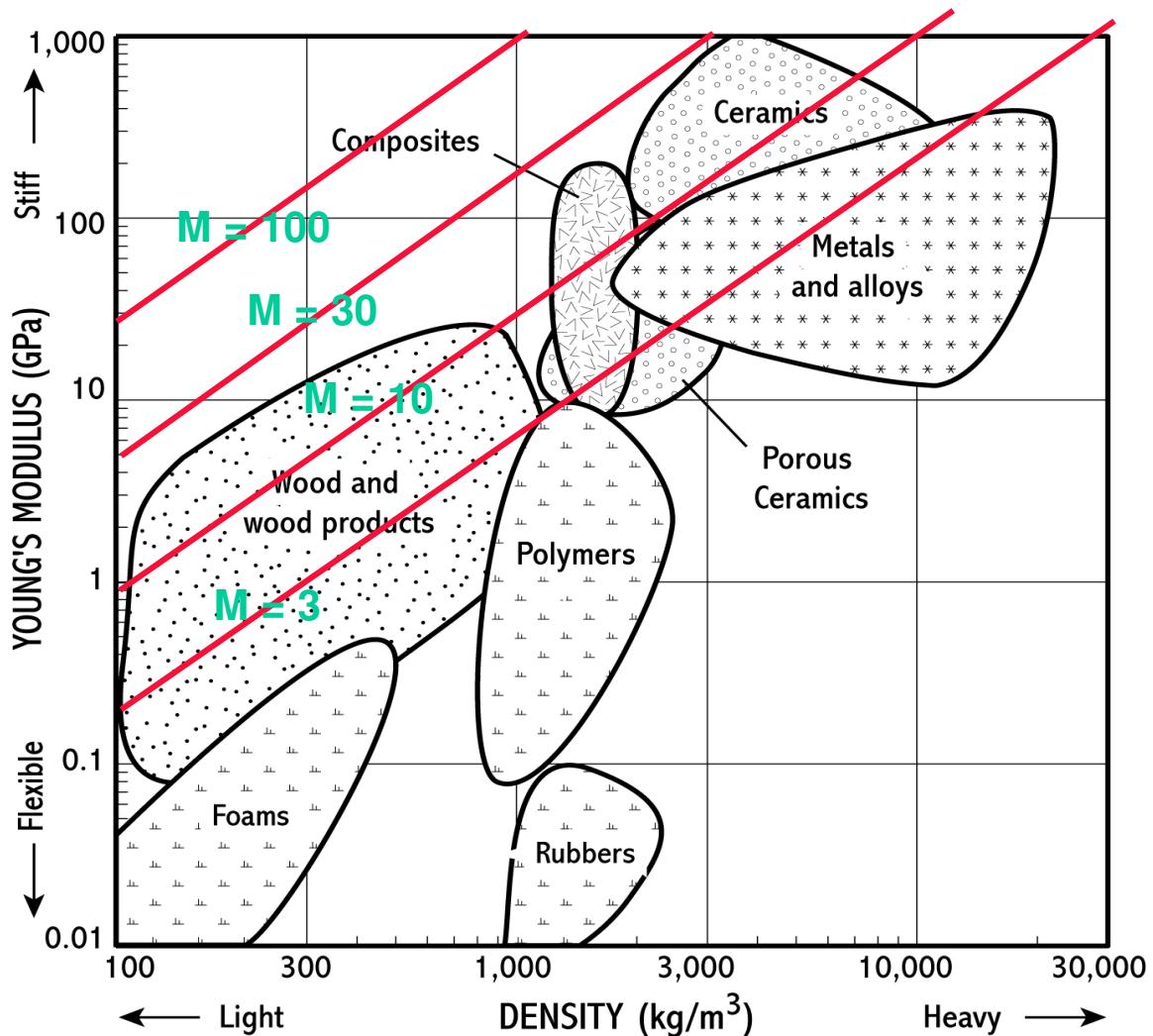


After M.F. Ashby

All parallel lines have the same performance

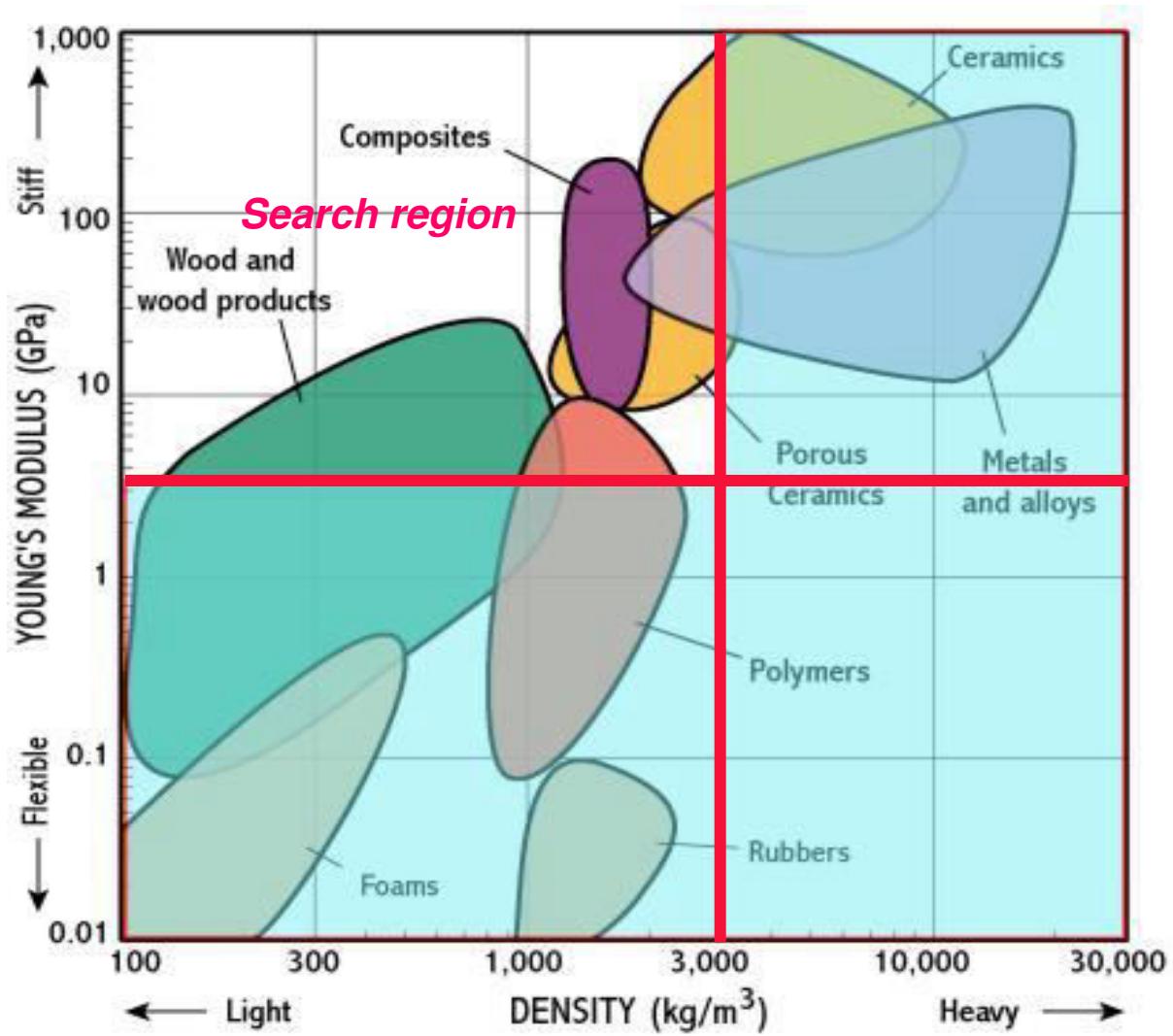
$M = 100$ is 1/10 the weight of $M = 10$

$M = 30$ is 1/3 the weight of $M = 10$



Constraints on the materials selection charts

- Selection of a material is influenced by constraints.
- Constraints appear as *horizontal* or *vertical lines* on the selection chart
- The primary constraints eliminate blocks of materials leaving a *viable search region*.
- The next step in selecting a material operates only on those materials which are left inside the search region



Red lines are
Constraints

After M.F. Ashby

Example

Use the E - ρ chart to find the material with modulus $E > 90$ GPa and density $\rho < 2$ Mg/m³

Young's modulus - Density

Technical
ceramics

These materials
can be selected for
the ρ constraint only

Young's modulus, E (GPa)

1000

100

10

1

0.1

0.01

$M = E^{1/2}$

10⁻³

10⁻⁴

0.01

0.1

1

10

Density, ρ (Mg/m³)

Composites -

Glass -

Al alloys

CFRP

Si₃N₄

B₄C

Multiple Constraints

- Most materials selection problems are over-constrained with more constraints than free variables.
- e.g; a component may require minimum weight, but with constraints on stiffness, strength and toughness which must also be met.
- This requires the use of several performance indices and several materials selection charts to identify the optimum material

- To solve this problem the following steps are considered:
 1. Identify the most important constraint [minimum weight without yielding (plastic deformation)] and identify the appropriate materials performance index. Ignore the remaining constraints.
 2. Use this to identify a subset of materials which maximise this performance index.
 3. Repeat for the next constraint(s) giving a second or a third performance index.

4. Then, identify a subset of materials which satisfy all performance indices.

- The second index may be plotted on the same chart as the first. The sector isolated above the two lines contains the subset of materials which satisfy the two criteria: $E^{1/2} / \rho > 8 \text{ GPa}^{1/2} / \text{Mg/m}^3$ and $E > 10 \text{ GPa}$.
- More often, however, the extra constraint involves a property which does not appear on the first chart.
- In this case, the members of the first subset of materials are tabulated, ranking them using a grid of performance index values

Example

1. Use the E - ρ chart to find the material with modulus $E > 100$ GPa and density $\rho < 2$ Mg/m³
2. Use the E - ρ chart to identify the subset of materials with both modulus $E > 100$ GPa and the performance index $M = E^{1/2} / \rho > (6 \text{ GPa})^{1/2} / (\text{Mg/ m}^3)$

Young's modulus - Density

Technical
ceramics

Composites -

Glass -

Si_3N_4

B_4C

Al alloys

CFRP

Young's modulus, E (GPa)

1000
100
10
1
 10^{-1}
 10^{-2}
 10^{-3}
 10^{-4}

These materials
can be selected for
the ρ constraint only

$$M = E^{1/2}$$

0.01

0.1

1

10

Density, ρ (Mg/m³)

Young's modulus - Density

Technical ceramics

Composites -

These materials
can be selected for
the $M = E^{1/2}/\rho$
constraint only

$$M = E^{1/2}$$

Density, ρ (Mg/m³)

Young's modulus, E (GPa)

1000
100
10
1
 10^{-1}
 10^{-2}
 10^{-3}
 10^{-4}

0.01 0.1 1 10

- The second index is used, with the appropriate chart, to identify a second subset of materials. Common members of the two subsets are identified and ranked according to their success in maximising the two performance indices.
- Consider a problem with one design goal, one free variable and two constraints.
- The result is two equations for the performance, each with the equation:

$$P = f_1 (F) \cdot f_2 (G) \cdot f_3 (M)$$

$$P = g_1 (F) \cdot g_2 (G) \cdot g_3 (M)$$

- The performance is maximised by choosing:
 1. Material with the largest “ $f_3(M)$ ”
 2. Material with the largest “ $g_3(M)$ ”
- The two equations must have equal values. The two performance indices are coupled.

$$\frac{f_3(M)}{g_3(M)} = \frac{g_1(F) \times g_2(G)}{f_1(F) \times f_2(G)}$$

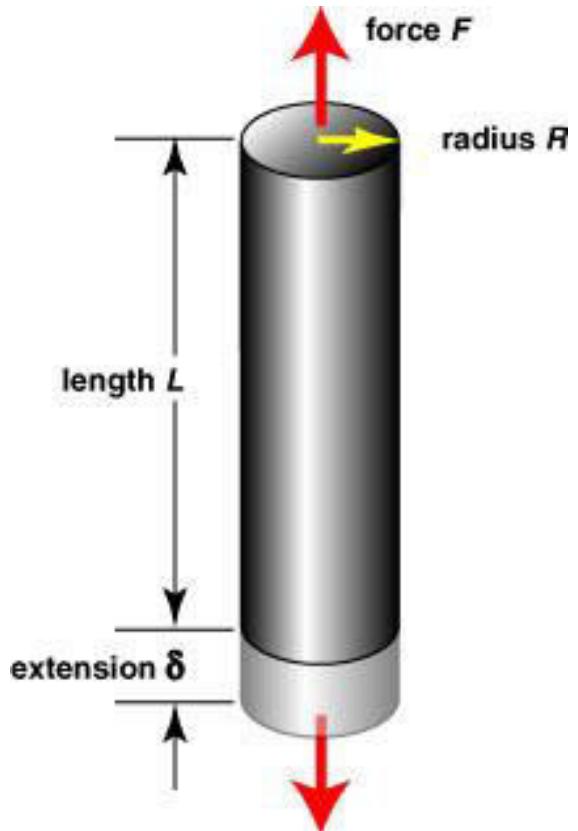
Example 4: Performance Index for a light, stiff and strong tie

- The tie (loaded in tension) is to support a load F , at minimum weight, without failing or extending by more than δ

- *Objective function*: reduce weight

$$m = A L \rho \quad (1)$$

- Specified dimensions: F and L
- Constraints: failure and stiffness
- Free variable: cross-sectional area, A .



After M.F. Ashby

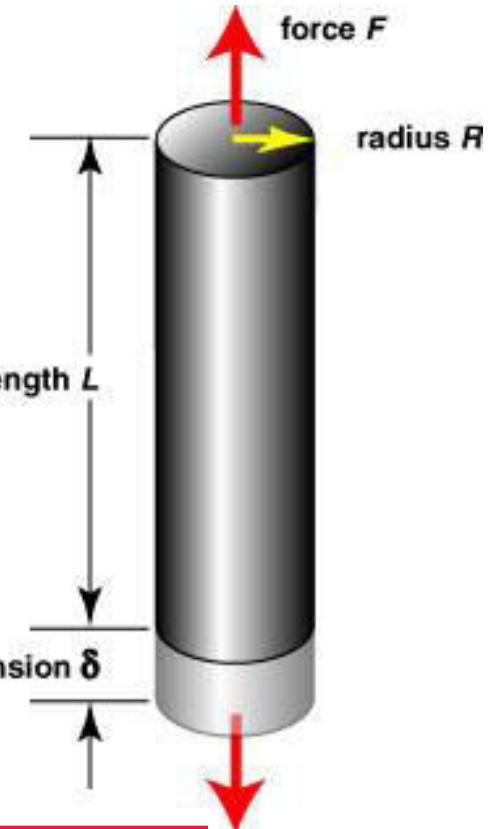
- We need to derive 2 performance indices
- M_1 for the stiffness constraint has already been derived in example 2 as:

$$M_1 = \frac{E}{\rho}$$

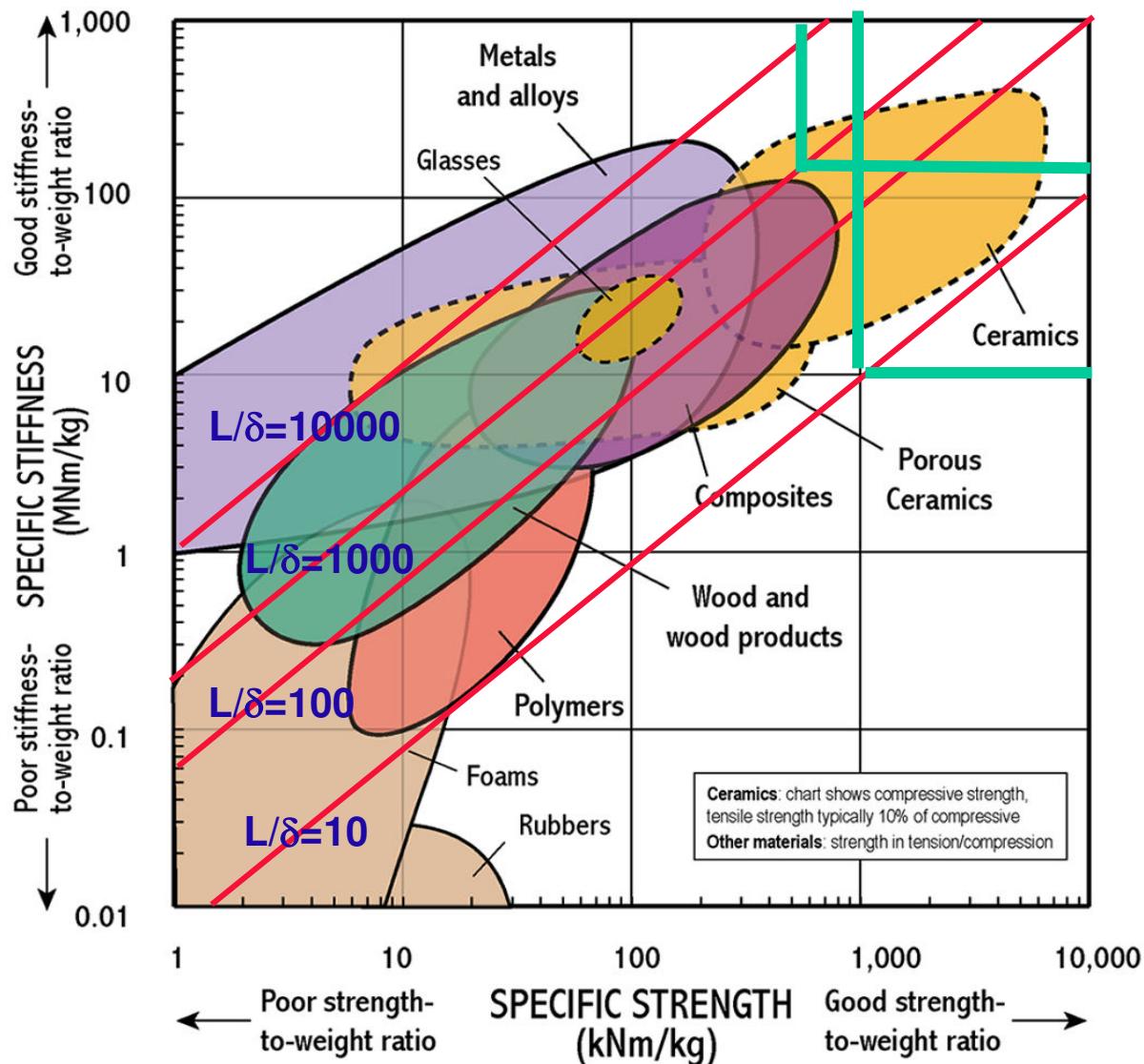
- M_2 for the failure constraint has also been derived in example 2 as:

$$M_2 = \frac{\sigma_f}{\rho}$$

- Since the weight is the same so that: $M_1 = M_2$
This is called the “*coupling equation*”



$$\frac{E/\rho}{\sigma_f/\rho} = \frac{L}{\delta}$$



After M.F. Ashby

Multiple Design Goals

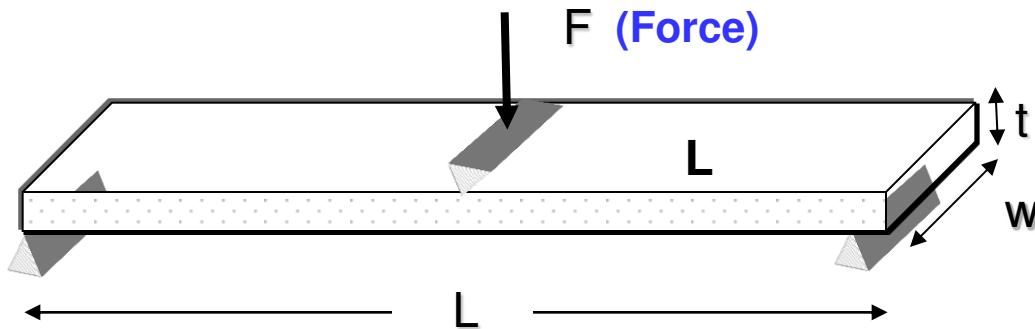
- For example, a design goal is to minimise weight, another is to minimise cost (how is weight to be compared to cost (they have different units?))
- The designer must assess the relative importance of all design goals by using “*weighting factors*” to each design goal
- First, the design goals are **ranked in order of importance**: a numerical factor of “10” is given to the most important goal and a factor of “1” is given to the least important

- The **performance index** for each design goal (starting with the most important) is determined
- Finally, the overall performance index is calculated by combining the performance index M obtained from each design goal
- Where $a_1 > a_2 > a_3$, are the weighting factors.

$$M = a_1 M_1 + a_2 M_2 + a_3 M_3 + \dots$$

- Alternatively a trade-off between the objectives should be used. This is illustrated in the next example.

Example 5: Stiff electronic casing (notebook) with minimum thickness and weight



FUNCTION

Bending

OBJECTIVES

1. Minimum thickness, t
2. Reduce weight: $m = AL\rho = w t L \rho$

CONSTRAINT

Stiffness $S = F/\delta = CEI/L^3$, $I = w t^3/12$

FREE VARIABLE

t

See example 3.1.5

OBJECTIVE 1

Minimum thickness, t

Using the constraint equation we get, t, as:

$$t = \left(\frac{12SL^3}{CEw} \right)^{1/3} \rightarrow M_1 = E^{1/3}$$

OBJECTIVE 2

Reduce weight, m

Using $m = w t L \rho$ and replacing t into the mass equation we get:

$$m = AL\rho = \left(\frac{12Sw^2}{C} \right)^{1/3} L^2 \left(\frac{\rho}{E^{1/3}} \right) \rightarrow M_2 = \frac{E^{1/3}}{\rho}$$

- For multiple objectives, we need to determine the relative performance indices.
- That is, suppose the casing is currently made of material M_0

1. The thickness of a casing made from an alternative material M , will be different from that made of material M_0 by the factor:
2. The mass of a casing made from an alternative material M , will be different from that made of material M_0 by the factor:

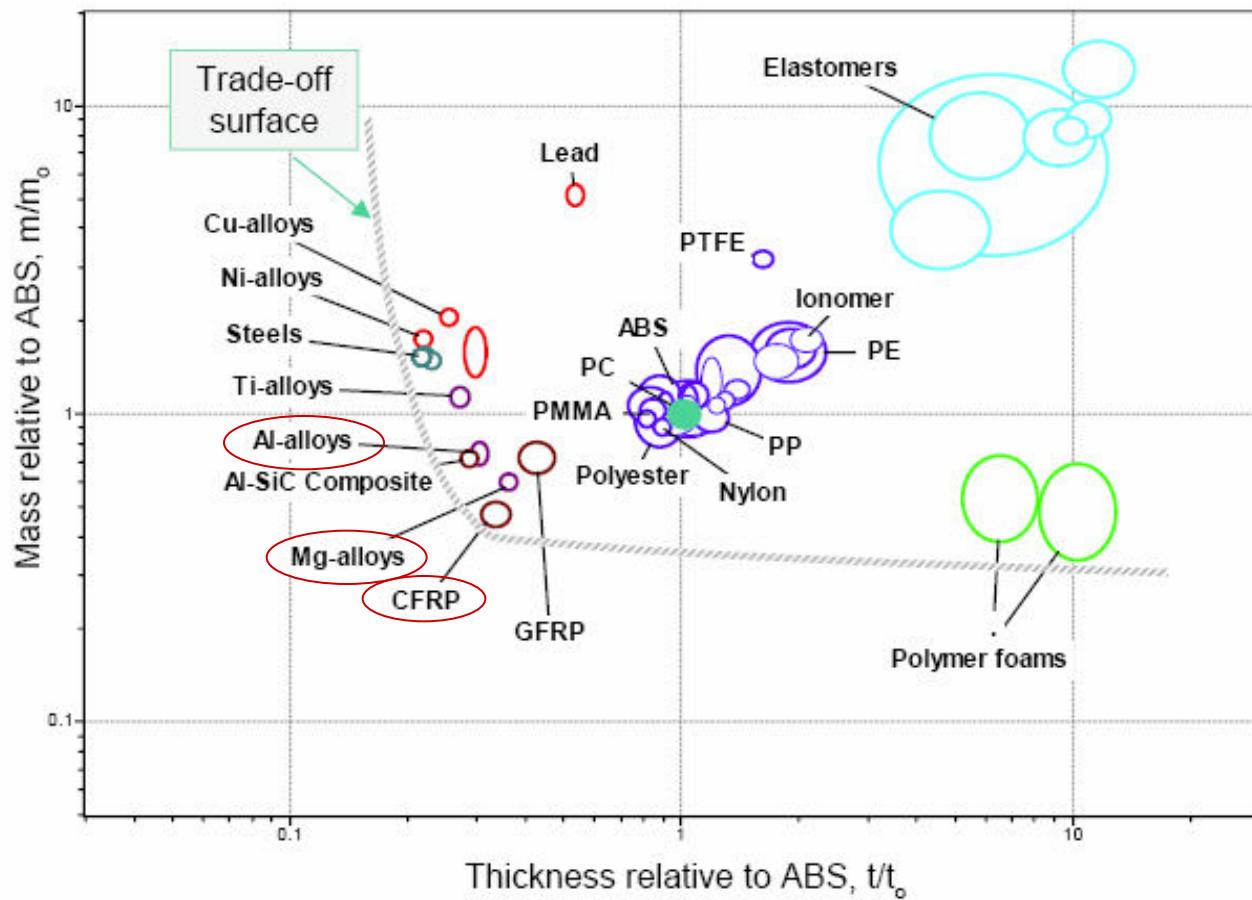
$$\frac{t}{t_0} = \left(\frac{E_0}{E} \right)^{1/3}$$

$$\frac{m}{m_0} = \left(\frac{\rho}{E^{1/3}} \right) \left(\frac{E_0^{1/3}}{\rho_0} \right)$$

- The trade-off between thickness and mass can be determined using the chart

$$\frac{t}{t_0} \quad \text{and} \quad \frac{m}{m_0}$$

TRADE-OFF PLOT



POSSIBLE MATERIALS: CFRP, Al & Mg alloys (Offer low mass at minimum thickness)

MATERIALS SELECTION CHARTS

